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<p>(54) Title: ALLYL-EPOXY IPN</p>			
<p>(57) Abstract</p> <p>The invention pertains to an interpenetrating polymer network (IPN) composed of (1) epoxy network forming compounds comprising: (a) polyfunctional epoxy compounds (epoxy resin); (b) polyfunctional aromatic hydroxyl compounds; (2) allyl network forming compounds; in which the (1):(2) weight ratio is in the range of 95:5 to 40:60, and the epoxy network forming compounds (1a) and (1b) are in a non-stoichiometric ratio to each other, such that the percentage of stoichiometry is in the range of 10 to 80 %. The percentage of stoichiometry is defined as 100 % times the quotient of the number of hydroxyl equivalents and the number of epoxy equivalents, i.e., eq. OH/eq. epoxy x 100 %. Such IPNs are especially suitable for use in the electronics industry and exhibit a favourable, high Tg and a low TCE. This also applies in the case of comparatively high percentages of epoxy resin giving optimum peel strength. The epoxy resin preferably is based on the diglycidyl ether of Bisphenol-A, while the allyl compound is triallyl cyanurate (TAC) or triallyl isocyanurate (TAIC).</p>			

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ALLYL-EPOXY IPN

The invention pertains to an interpenetrating polymer network (IPN) composed of

5 (1) epoxy network forming compounds comprising
(a) polyfunctional epoxy compounds;
(b) polyfunctional aromatic hydroxyl compounds;
(2) allyl network forming compounds;

in which the (1):(2) weight ratio is in the range of 95:5 to 40:60.

10 Such IPNs have very favourable properties, particularly for use in the electronics industry, and are known from US 5,210,157, which US patent specification is to be considered incorporated herein by reference.

15 The favourable properties of said known IPNs are attributable largely to the constituents selected (cyclic moiety-containing allyl compounds which are cross-linked in the presence of a radical initiator and epoxy resin cross-linked with the aid of a polyhydric phenol). Very good properties are obtained with the known IPNs when approximately 20 40-60 weight percent of the IPN is composed of epoxy resin, with optimum results being obtained when triallyl cyanurate monomer or prepolymer (TAC) or triallyl isocyanurate (TAIC) is used as the allyl compound. This shows itself, e.g., in a high Tg. The Tg, it turns out, is affected by, among others, the allyl to epoxy ratio, it being the 25 case that a larger amount of epoxy resin will lead to a lower Tg. The Tg is also affected by the type of cyclic moiety-containing allyl compound. For instance, the known IPNs tend to have a lower Tg when the allyl compound selected is diallyl phthalate (instead of, say, triallyl cyanurate).

30 It is now desired to provide IPNs which have the favourable properties, particularly for the electronics industry, of the aforementioned known IPNs; but which in addition show enhanced

5 properties (notably: high Tg, low thermal expansion, sufficient fire retardancy at a lower bromine content, high copper peel strength) not only for the preferred embodiments of the known IPNs, but especially for compositions with a comparatively large epoxy resin constituent or for compositions (also) containing allyl compounds other than TAC or TAIC.

10 Further prior art background is formed by US 4,661,568 (Koenig), WO 82/1877 (Whiteside), neither of which relates to IPNs but to epoxy resin, US 4,755,571 (Irving), and GB 994,484.

15 Described in Koenig is an epoxy resin composition comprising an epoxy resin, a solvent, and a hardener which is the reaction product of a polyhydric phenol and a hexa-alkyl ether of a particular methylol melamine. The disclosed epoxy resins have a comparatively high Tg (150°-170°C) and are utilised in electronic laminates. The ratio of phenolic hydroxyl to epoxy is in the range of 0.5:1 to 2:1., preferably in the range of 0.8:1 to 1.2:1. A drawback to the described 20 hardener consists in that the discharge of methanol may cause objectionable blistering. In addition, Koenig's prepreg manufacture employs a temperature which is unfavourably low in view of the rate of output.

25 Whiteside teaches a method of increasing the molecular weight of epoxy resin by reacting an epoxy resin composed of a glycidyl ether of a dihydric phenol having more than one glycidyl ether group per molecule with a dihydric phenol in the presence of a phosphonium catalyst. The ratio of phenolic hydroxyl to epoxy is such that the resulting 30 reaction product will have a theoretical epoxy content (in percent) of from 2.7 to 14. This means (as the examples show), an epoxy equivalents to OH equivalents ratio in the range of 3:1 to 4:1.

Irving describes an IPN based on an anaerobically polymerisable mixture comprising a free radical polymerisable compound, a radical initiator, an accelerator, and an epoxy resin cured with the aid of a base, a polymercaptan, or a polyhydric phenol. Irving makes no mention of IPNs based on allyl compounds.

GB 994,484 teaches a cured composition which in the uncured state comprises an epoxy novolac, the dianhydride of pyromellitic acid, and an unsaturated reactive diluent. The reactive diluent may be triallyl cyanurate, providing no polyol accelerators are employed.

From JP-Hei-4-216818 resin compositions are known that comprise, int.al., an epoxy terminated allyl-containing prepolymer and a hydroxyl terminated allyl-containing prepolymer.

JP-Hei-4-108860 teaches a thermosetting composition obtained by blending a thermosetting resin such as an epoxy resin with triallyl isocyanurate and triallyl isocyanurate prepolymer. The disclosure leaves open desires similar to those left open by the disclosure of US 5,210,157 cited above.

The discussed literature references teach neither IPNs of the aforementioned type, nor the desired improvements of these IPNs. These improvements are provided by the present invention. To this end the invention consists in that in an IPN of the aforementioned known type the epoxy network forming compounds (1a) and (1b) are in a non-stoichiometric ratio to each other, such that the percentage of stoichiometry is in the range of 10 to 80%, the percentage of stoichiometry being defined as 100% times the quotient of the number of hydroxyl equivalents and the number of epoxy equivalents.

The epoxy network in the present IPNs is built up from polyfunctional epoxy compounds (epoxy resin) cross-linked with polyfunctional aromatic hydroxyl compounds.

By the term "epoxy resin" is meant a curable composition of oxirane ring-containing compounds. Such compounds have been described in C.A. May, Epoxy Resins, 2nd Edition (New York & Basel: Marcel Dekker Inc., 1988).

5 As examples of epoxy resins may be mentioned phenol types, such as those based on the diglycidyl ether of Bisphenol-A, on polyglycidyl ethers of phenol-formaldehyde novolac or cresol-formaldehyde novolac, on the triglycidyl ether of tris(p-hydroxyphenol)methane, or on the tetraglycidyl ether of tetraphenyl ethane; amine types, such as those 10 based on tetraglycidyl methylene dianiline or on the triglycidyl ether of p-aminoglycol; cycloaliphatic types, such as those based on 3,4-epoxycyclohexylmethyl-3,4-epoxycyclohexane carboxylate.

15 By the term "epoxy resin" are also meant reaction products of compounds containing an excess of epoxy (e.g., of the types indicated above) and aromatic dihydroxy compounds. These dihydroxy compounds may be halogen substituted.

20 Preference is given to epoxy resins of the phenol type, especially because of their low price.

It should be noted that, usually, epoxy resins are illustrated by a single unequivocal structural formula. Differing products resulting 25 from side reactions which occur in the preparation of epoxy resins should, as the skilled person knows, be considered to be included therein. As these side products form a standard constituent of cured epoxy resins, so they make up a standard constituent of the IPNs according to the invention.

30 Generally, an accelerator is employed when cross-linking the epoxy resin. As suitable accelerators may be mentioned imidazoles, more particularly alkyl substituted imidazoles such as 2-methyl imidazole and 2-ethyl-4-methyl imidazole, and tertiary amines such as benzyl dimethyl amine.

5 The quantity in which such an accelerator is employed is dependent on the type of epoxy resin, the type of cross-linking agent, and the type of accelerator, but it will generally be in the range of 0,01 to 5 wt.%, calculated on the overall weight of epoxy resin and cross-linking agent.

10 Examples of polyfunctional aromatic hydroxyl compounds include dihydroxy compounds having formulae such as given in US Patent Specification 5,210,157 incorporated herein by reference. Further, novolac resins such as phenol/formaldehyde, cresol/formaldehyde, or phenol/p-hydroxybenzaldehyde may act as polyfunctional aromatic hydroxyl cross-linking agents.

15 The preferred cross-linking agents for the epoxy resin are sulphone diphenol and tetrabromo-Bisphenol-A.

20 A key element of the present invention resides in that the polyhydric phenol cross-linking agent is used in such an amount as will result in a hydroxy groups to epoxy groups ratio in the range of 0.1:1 to 0.8:1 (10 to 80% stoichiometry). When there is more than 80% stoichiometry, the Tg enhancing effect according to the invention occurs hardly if at all, while with less than 10% stoichiometry phase separation of the two networks is observed, resulting in inferior thermal properties. Moreover, too much excess epoxy will give rise to insufficient fire retardancy.

25 Preferably, the percentage of stoichiometry is in the range of 30 to 70%, primarily because in this range favourable, low thermal coefficients of expansion (TCEs) are obtained, as well as, of course, a high Tg. The most favourable combination of high Tg and low TCE is achieved when the percentage of stoichiometry is in the range of 40 to 60%.

As examples of suitable allyl monomers turned into an allyl polymer network by means of radical cross-linking may be mentioned triallyl cyanurate (TAC), triallyl isocyanurate (TAIC); aromatic polyallyl esters, such as diallyl phthalate, diallyl isophthalate, triallyl 5 trimellitate, tetraallyl pyromellitate, diallyl tetrabromophthalate; aliphatic polyallyl esters, such as diallyl adipate, diallyl maleate, diallyl fumarate, and polyallyl carbonates such as diethylene glycol diallyl carbonate.

10 Alternatively, mixtures of allyl monomers and allyl prepolymers may be employed in the preparation of IPNs according to the invention.

15 For partial replacement of the polyallyl compounds in the IPN use may be made of aromatic difunctional methacrylates such as described in US 5,210,157. The use of 2,2-di(4-methacryloxy-ethoxyphenyl)propane (BMEPP) is preferred.

20 However, it is of importance to have the allyl compounds present in the IPNs according to the invention in an amount of at least 5% (percent by weight of the solvent-free resin). Preferably, these allyl compounds are cyclic moiety-containing allyl compounds, and even when the IPN contains more than 5% of allyl constituents, it is desired to have at least 5% of cyclic moiety-containing allyl compounds present in the IPN, notably nitrogen-containing allyl compounds such as TAC 25 and TAIC.

30 Polymerisation of the polyallyl compounds is generally carried out under the influence of an initiator, which will commonly be used in a ratio of 0.1-5 wt.% vis-à-vis the allyl compound. As suitable initiators may be mentioned peroxides, such as t-butylperoxy benzoate, t-butylperoxy-3,5,5-trimethyl hexanoate, and benzoyl peroxide. Alternatively, it is possible to have thermal polymerisation without an initiator.

Generally, an organic solvent will be used in the preparation of IPN resins according to the invention. An advantage of the use of TAC as an IPN constituent is that it can also act as a solvent. If an additional solvent is employed, the epoxy resin, the cross-linking agent, and the polyallyl compound must be soluble therein, while the solvent itself has to be sufficiently volatile to volatise prior to or during partial curing of the IPN, or prior to final curing.

Suitable solvents are, e.g., dimethyl formamide; glycol ethers, such as ethylene or propylene glycol monoethyl ether, and esters thereof such as ethylene glycol monoethyl ether acetate; ketones, such as methyl isobutyl ketone, methylethyl ketone, acetone, and methyl isopropyl ketone; aromatic hydrocarbons such as toluene and xylene. Use may also be made of mixtures of solvents. The preferred solvents are ketones, notably acetone and methylethyl ketone, and mixtures thereof with ethers, notably propylene glycol monoethyl ether.

As also holds for the known IPNs, halogen substituents may be introduced into the various IPN components. This is to render the IPN sufficiently fire retardant. Preferably, bromine is employed to this end. In the case of the IPNs described in US 5,210,157, the use of TAC or TAIC is known to give good fire retardancy at a lower bromine percentage (in the case of an IPN comprising 70% of TAC, ca. 10 wt.% of bromine instead of ca. 18 wt.%), which is very pleasant for environmental reasons. For the IPNs according to the present invention it was found that, because of the use of non-stoichiometric epoxy resin, less than about 14 wt.% of bromine will suffice also in embodiments containing more than 50% of epoxy resin (and, hence, comparatively little TAC). For attaining fire retardancy at a low bromine percentage it is preferred to have a percentage of stoichiometry in the range of 30 to 40%.

The invention further pertains to laminates for use in the electronics industry into which IPNs of the type described above have been incorporated.

5 Laminates for use in the electronics industry (notably for printed wiring boards) are generally manufactured by impregnating a supporting or reinforcing material (usually on a glass fibre basis, either in fabric form or in the form of a cross-ply laminate of unidirectionally oriented parallel filaments) with a resin, followed by wholly or 10 partially curing the resin. The latter form is the most conventional one, and a fabric impregnated with a partially cured resin is commonly called a prepreg. Manufacturing a printed wiring board from a fabric prepreg involves laminating one or more layers of the prepreg with one or more layers of, say, copper.

15 As a rule, the resin employed will be an epoxy resin. Presently, the standard in actual practice is the FR4 laminate, which is based on a brominated epoxy resin prepared from a diglycidyl ether of Bisphenol-A and tetrabromo Bisphenol-A, dicyanodiamide as hardener, an organic 20 solvent, an accelerator, and a catalyst. Such an epoxy resin has the drawback of a low T_g (110°-135°C), however, and there is also a tendency on the part of the dicyanodiamide to crystallise in the resin and in the prepreg made from the resin.

25 The IPN resins according to the invention are highly suited to be used for the impregnation of, int. al., fabric and cloth of a wide range of materials, such as glass, quartz, carbon, aramid, and boron fibres, especially for making laminates for printed wiring boards, for which application the IPN is preferably employed in combination with a glass 30 fabric.

As is already known from US 5,210,157, when the copper peel strength is of considerable importance, it is preferred to incorporate the

largest possible epoxy resin constituent into IPNs of the allyl/epoxy type. Whereas in the known IPNs the optimum allyl polymer to epoxy resin ratio is in the range of 30:70 to 40:60 so as to retain favourable thermal properties, the IPNs according to the present invention not only display superior thermal properties at these ratios but also permit the incorporation of a larger epoxy resin constituent into the IPN while retaining these thermal properties. In this connection an epoxy resin to allyl compounds weight ratio in the range of 90:10 to 60:40 is preferred for IPNs to be used in metallised laminates.

10

Furthermore, the IPN resins according to the invention may be used wherever conventional epoxy resins are employed: as glue, coating, moulding resin, embedding resin, encapsulating resin, sheet moulding compound, bulk moulding compound.

15

In addition to the aforementioned application as a composite for printed wiring boards the IPN resins according to the invention may be employed to make composites for use in, say, the construction business and the aviation and car industries.

20

The manufacture of suitable structural composites may be in the known manner, e.g., by impregnating reinforcing material with molten or dissolved resin or by means of resin transfer moulding, filament winding, pultrusion, or RIM (reaction injection moulding).

25

The IPN resins according to the invention may contain such conventional additives as dyes or pigments, thixotropic agents, flow regulators, and stabilisers.

30

The invention will be illustrated with reference to the following unlimitative examples below.

Example 0

Preparation of the TAC prepolymer used in the examples

5 To 1.6 kg of molten TAC (= triallyl cyanurate) monomer in a reactor (fitted with a cooler, a stirrer, and a feeder funnel) were added 252 g of MEK and 20 g of carbon-tetrabromide. Next, the contents of the reactor were heated to 95°C, with stirring, and a solution of 28.0 g of dioctanoyl peroxide in 210 g of MEK (methylethyl ketone) was added dropwise over a period of two hours. After a total reaction time
10 at 95°C of six hours 0.16 g of 2,6-di-tertiary butyl-p-cresol was added to the solution, which was then cooled to room temperature.

15 The 78% TAC prepolymer solution comprising 22 wt.% of MEK had a viscosity of 150 mPa.s. HPLC measurement showed 40% of the monomer to have been converted into oligomer having, relative to polystyrene standards, a number average molecular weight of 7000 and a degree of dispersion of 20.

20 Example 1

25 A mixture was prepared of 27.6 g (0.120 epoxy equivalents) of cresol formaldehyde novolac polyglycidyl epoxy resin (CNE for short, with an epoxy equivalent weight of 230 and a functionality of 4), 32.4 g (0.119 hydroxyl equivalents) of tetrabromobisphenol A, 22.0 g of MEK, and 51.3 g of a TAC prepolymer solution prepared as specified in Example 0. The part by weight of TAC prepolymer in the mixture was 40%, the part by weight of epoxy plus tetrabromobisphenol A (TBBPA) was 60%. The percentage of stoichiometry, i.e., the ratio of hydroxyl equivalents to epoxy equivalents times 100%, was 99.2%. To the solution, which contained 25.0 wt.% of MEK, was added 0.6 g of a 10 wt.% solution of 2-methyl imidazole in 2-methoxy-1-propanol and subsequently 0.4 g of tertiary-butyperoxy benzoate. Next, the resin
30

solution was poured into aluminium dishes in such a way as to give a layer thickness for the resin solution of 0.5 to 1 mm. The samples were then heated to 60°C in a forced-circulation air oven and kept at 60°C for one hour. The temperature of the oven was then raised to and kept for 30 minutes at 100°C, followed by one hour at 120°C and, 5 finally, one hour at 170°C. After the orangish-brown, homogeneously transparent plates had been cooled slowly and released from the mould, the samples were post-cured for a further two hours at 200°C and then cooled slowly to room temperature. The properties of the flat, cured 10 plates are listed in Table 1 under composition A.

The same preparative process was used for compositions B through H, which are also listed in Table 1. Compositions A through H all have 15 the same portion of TAC prepolymer but different percentages of stoichiometry.

Example 2

Prepared were a prepreg and laminates based on a resin solution 20 composed of:

- 580 g of a 65%-solution of 233 g of CNE epoxy resin (the same type as in Example 1) and 144 g of tetrabromobisphenol A in MEK;
- 322 g of a 78%-solution of TAC prepolymer in MEK;
- 3.8 g of a 10%-solution of 2-methyl imidazole in 2-methoxy-1- 25 propanol; and
- 2.5 g of t-butylperoxy benzoate.

The 70%-resin solution, which contained 40 parts of TAC prepolymer 30 versus 60 parts of epoxy plus TBBPA, had a viscosity of 100 mPa.s determined in accordance with the instructions by Brookfield at a temperature of 20°C. The quantity of TBBPA hydroxyl groups was 52% of the stoichiometric amount required for the presented epoxy groups.

5 In a laboratory treater E-glass fabric of type 7628 (finishing agent Z 6040) was continuously impregnated with the resin solution at a temperature of 170°C, with the solvent being removed and the resin being partially cured to the B stage. The appearance of the prepgs
10 was excellent and they were non-sticky. The rate at which the fabric was fed to the treater was set such as to give a resin weight percentage and a percentage of resin flow in the prepg of 44 ± 3 and 22 ± 3, respectively. The weight percentage and the percentage of flow of the resin at 171°C were determined conventionally in accordance with IPC methods TM 650 2.3.16 and 2.3.17 (IPC = Institute for 15 interconnecting and packaging electronic circuits).

15 Eight prepgs stacked one on top of the other were moulded in a vacuum press at a specific pressure of 15 atm. and a temperature of 171°C for 60 minutes. Heating and cooling was at a rate of 5°C/minute. In this manner both a laminate coated on either side with copper (1 ounce, electrodeposited type) and an uncoated laminate having a thickness in the range of 1.50 to 1.60 mm were made. All laminates 20 were subjected to two hours of additional post-curing in an oven at 200°C.

25 The properties of the laminate and of reference laminate 1 are listed in Table 2. The reference laminate, which was prepared as specified in Example 2, is based on the same composition as in Example 2, except that 89% of the stoichiometric amount of TBBPA was employed.

Example 3

30 In a manner analogous to that described in Example 2 several laminates were made, with the TAC prepolymer content in the resin being varied vis-à-vis the CNE epoxy plus TBBPA content, and with the percentage of stoichiometry being kept constant at 52%. The data is listed in Table 3 along with that of two reference examples, viz. 2 and 3.

Example 4

Based on phenol-formaldehyde novolac polyglycidyl epoxy resin (FNE for short) having an average epoxy functionality of 3.5 and an epoxy equivalent weight of 178, a resin was formulated as follows:

5 - 2151 g of a 70%-solution of 855 g of FNE epoxy hars and 645 g of TBBPA in MEK;
- 1283 g of a 78%-solution of TAC prepolymer in MEK;
- 15 g of a 10%-solution of 2-ethyl,4-methyl imidazole in MEK;
10 - 10 g of t-butyperoxy benzoate.

The 73%-resin solution, which contained 40 parts of TAC prepolymer versus 60 parts of epoxy plus TBBPA, had a viscosity of 80 mPa.s determined in accordance with the instructions by Brookfield at a 15 temperature of 20°C. The quantity of TBBPA hydroxyl groups was 49% of the stoichiometric amount required for the presented epoxy groups.

In a manner analogous to that described in Example 2 this resin was processed into prepgs and laminates. Its composition and thermal 20 properties are compiled in Table 4 as Example 4A. This table also lists the composition and results for two similar resins, Examples 4B and 4C, characterised in that they had a stoichiometry percentage of 25% and 79%, respectively. It should be noted that in Example 4B the prepgs were moulded into a laminate in an autoclave, instead of in a 25 vacuum press as in the other examples, because the resin flow was too high and the desired thickness of 1.5 to 1.6 mm was therefore not achieved.

Example 5

30 A resin was formulated from:

- 3277 g of a 55%-solution of 1113 g of CNE epoxy resin and 687 g of TBBPA in MEK;
- 600 g of triallyl cyanurate monomer;

- 600 g of (ortho-)diallyl phthalate prepolymer (DAP prepolymer), commercially available from Osaka Soda Co., having \leq 3% monomer and an iodine number of 60;
- 18 g of a 10%-solution of 2-methyl imidazole in 2-methoxy-1-propanol;
- 5 - 12 g of t-butylperoxy benzoate.

10 The 67%-resin solution, which contained 20 parts of TAC monomer and 20 parts of DAP prepolymer versus 37.1 parts of epoxy and 22.9 parts of TBBPA, had a viscosity of 110 mPa.s determined in accordance with the instructions by Brookfield at a temperature of 23°C. The quantity of TBBPA hydroxyl groups was 52% of the stoichiometric amount required for the presented epoxy groups.

15 In a manner analogous to that described in Example 2 this resin was processed into prepregs and laminates. The results are given in Table 5.

20

25

30

Table 1

	<u>Composition</u>	<u>A</u>	<u>B</u>	<u>C</u>	<u>D</u>	<u>E</u>	<u>F</u>	<u>G</u>	<u>H</u>
5	% stoichio-metry	99.3	78.5	57.4	52.2	36.8	26.1	5.3	0
	Composition								
	% CNE epoxy res.	27.6	31.1	35.7	37.1	41.9	45.8	56.5	60.0
	% TBBPA	32.4	28.9	24.3	22.9	18.1	14.2	3.5	--
	% TAC prepol.	40.0	40.0	40.0	40.0	40.0	40.0	40.0	40.0
10	epoxy equivalents	0.120	0.135	0.155	0.161	0.182	0.199	0.246	0.261
	hydroxyl equivalents	0.119	0.106	0.089	0.084	0.067	0.052	0.013	0
	% bromine ¹	19.5	17.5	14.7	14.0	11.1	8.8	2.6	0.5
15	Tg (°C) by TMA	155	173	190	190	190	185	2Tg ¹ s ²	2Tg ¹ s ³
	T.C.E. (ppm/°C average over 20°-250°C)	130	130	100	102	110	120	190	≥210
20	TGA (N2 atm.)								
	* loss at 300°C (%)	1.7			1.6			1.5	1.5
	* decomposition maximum (°C)	325			326			383	405;537
	* residual at 650°C (%)	25			24.2			17.0	0.5
25	flame test, fire retardant?	yes	yes	yes	yes	yes	yes/no	no	no

¹) calculated bromine content (%) in composition exclusive of MEK

²) 2 Tgs, 170° and 220°C

³) 2 Tgs, sample is still curing: first run 130° and 220°C, second run 170° and 220°C

Table 2

	Example 2	Reference 1
5	Resin composition:	
	% TAC prepolymer	40
	% CNE epoxy resin	37.1
	% TBBPA	22.9
10	% stoichiometry	52
	% bromine	13.9
	Laminate:	
	Tg (°C)	
15	* by TMA	185
	* DMTA (damping maximum)	235
	T.E.C.z. (ppm/°C) average (over 20°-250°C)	100
20	fire retardancy UL94, class	V0
		V0

Table 3

		Ex. 3A	Ex. 3B	Ex. 2	Ref. 2	Ref. 3
5	Resin composition:					
	% TAC prepolymer	10	20	40	20	0
	% CNE epoxy resin	55.6	49.4	37.1	39	62.8
	% TBBPA	34.4	30.6	22.9	41	37.2
10	% stoichiometry	52	52	52	89	50
	% bromine	20.3	18.3	14	24.4	21.9
15	Laminate properties:					
	Tg (°C)					
	* by TMA	165	175	185	153	138
	* DMTA (damping max.)	185	200	235	195	160
20	T.E.C.z (ppm/°C) average (over 20°-250°C)	145	130	100	155	200
	dielectric constant at 1 MHz	4.3	4.3	4.3	4.4	4.4
25	dissipation factor at 1 MHz	0.011	0.012	0.011	0.009	0.012
	water absorption %	0.15	0.12	0.15	0.10	0.10
	dichloromethane absorption after 30'	0.07	0.09	0.10	0.05	0.21
30	Copper peel strength (N/cm) - as such	15.8	12.6	14.3	11.4	17.4
	- after solder bath 10" (288°C)	15.8	12.2	14.5	12.2	17.2
	Fire retardancy UL94, class	VO	VO	VO	VO	VO

Table 4

		Example 4A	Example 4B	Example 4C
5	Resin composition:			
	% TAC prepolymer	40	40	40
	% FNE epoxy resin	34.2	43.5	27.2
	% TBBPA	25.8	16.5	32.8
10	% stoichiometry	49	25	79
	% bromine	15.7	10.2	19.8
	Laminate:			
	Tg (°C)			
15	* by TMA	177	177	164
	* DMTA (damping maximum)	220	200	210
	T.E.C.z (ppm/°C) average (over 20-250°C)	100	100	105

Table 5

		Example 5
5	Resin composition:	
	% TAC monomer	20
	% DAP prepolymer	20
	% GNE epoxy resin	37.1
	% TBBPA	22.9
10	% stoichiometry	52
	% bromine	14
	Laminate properties:	
15	Tg (°C)	
	* by TMA	157
	* DMTA (damping maximum)	190
	T.E.C.z (ppm/°C)	150
	average (over 20-250°C)	
20	dielectric constant at 1 MHz	4.2
	dissipation factor at 1 MHz	0.012
	water absorption %	0.11
25	dichloromethane absorption after 30'	0.03
	Copper peel strength (N/cm)	
	- as such	14.1
	- after solder bath 10" (288°C)	13.1
30	Fire retardancy UL94, class	VO

Claims

1. An interpenetrating polymer network (IPN) composed of
 - 5 (1) epoxy network forming compounds comprising
 - (a) polyfunctional epoxy compounds;
 - (b) polyfunctional aromatic hydroxyl compounds;
 - (2) allyl network forming compounds;
in which the (1):(2) weight ratio is in the range of 95:5 to
 - 10 (1a) and (1b) are in non-stoichiometric ratio to each other, such that the percentage of stoichiometry is in the range of 10 to 80%, the percentage of stoichiometry being defined as 100% times the quotient of the number of hydroxyl equivalents and the number of epoxy equivalents.
2. An IPN according to claim 1, characterised in that the percentage of stoichiometry is in the range of 30 to 70%.
- 20 3. An IPN according to claim 2, characterised in that the percentage of stoichiometry is in the range of 40 to 60%.
4. An IPN according to any one of the preceding claims, characterised in that the epoxy network contains a fire retardancy providing
 - 25 amount of bromine.
5. An IPN according to claim 4, characterised in that the percentage of stoichiometry is in the range of 30 to 40%, and the percentage of bromine in the IPN does not exceed 15 weight%.
- 30 6. An IPN according to any one of the preceding claims, characterised in that it comprises at least 5 wt.% of a cyclic moiety-containing allyl compound.

7. An IPN according to claim 6, characterised in that it comprises triallyl cyanurate as cyclic moiety-containing allyl compound.
- 5 8. A laminate comprising at least a plastics layer and a layer of metal, characterised in that the plastics layer is composed of an IPN according to any one of the preceding claims which may be fibre-reinforced or not.
- 10 9. A laminate according to claim 8, characterised in that the epoxy compounds to allyl compounds weight ratio in the IPN is in the range of 90:10 to 60:40.
- 15 10. A printed wiring board (PWB) manufactured from a laminate according to claim 8 or 9.

INTERNATIONAL SEARCH REPORT

Int'l Application No
PCT/EP 94/02664A. CLASSIFICATION OF SUBJECT MATTER
IPC 6 C08F283/10 B32B27/38 H05K1/03

According to International Patent Classification (IPC) or to both national classification and IPC

B. FIELDS SEARCHED

Minimum documentation searched (classification system followed by classification symbols)
IPC 6 C08F B32B H05K

Documentation searched other than minimum documentation to the extent that such documents are included in the fields searched

Electronic data base consulted during the international search (name of data base and, where practical, search terms used)

C. DOCUMENTS CONSIDERED TO BE RELEVANT

Category *	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
X	<p>DATABASE WPI Section Ch, Week 9238, Derwent Publications Ltd., London, GB; Class A21, AN 92-311923 'epoxy contained resin compsn. for package of semiconductor -comprises allyl contained prepolymer contg. both terminals epoxy ... & JP,A,4 216 818 (SUMITOMO BAKELITE CO.) 6 August 1992 cited in the application see abstract</p> <p>---</p> <p style="text-align: center;">-/-</p>	1,2,4,5

 Further documents are listed in the continuation of box C. Patent family members are listed in annex.

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1

Date of the actual completion of the international search

16 November 1994

Date of mailing of the international search report

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INTERNATIONAL SEARCH REPORT

Inte: Application No

PCT/EP 94/02664

C(Continuation) DOCUMENTS CONSIDERED TO BE RELEVANT

Category	Citation of document, with indication, where appropriate, of the relevant passages	Relevant to claim No.
Y	PATENT ABSTRACTS OF JAPAN vol. 016, no. 356 (C-0969) 31 July 1992 & JP,A,41 008 860 (MATSUSHITA ELECTRIC WORKS LTD) 9 April 1992 cited in the application see abstract ---	1-10
Y	EP,A,0 413 386 (AKZO N.V.) 20 February 1991 cited in the application see claims; examples & US,A,5 210 157 (AKZO) cited in the application -----	1-10

INTERNATIONAL SEARCH REPORT

Information on patent family members

Inte. onal Application No

PCT/EP 94/02664

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		JP-A-	3097721	23-04-91
		US-A-	5210157	11-05-93
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		DE-D-	69008270	26-05-94
		DE-T-	69008270	27-10-94
		EP-A-	0413386	20-02-91
		JP-A-	3097721	23-04-91
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